



# CAB530 - July 9, 2019

Item # CAB530 was discontinued on July 9, 2019. For informational purposes, this is a copy of the website content at that time and is valid only for the stated product.

#### LASER DIODE CURRENT / TEC CONTROLLER - ITC5000 SERIES

- **▶** Current & Temperature Control
- ▶ 3 Current Ranges
- ► Very Low Noise and Drift
- ► For All Laser Diode Polarities

Easy-to-Use Graphical Interface (PC Not Included)





Modules in TXP5016 Chassis



**Hide Overview** 

#### OVERVIEW

#### Three Versions to Choose from:

- ITC5022: Laser Diode Current/TEC Controller ±200 mA / ±1.5 A
- ITC5052: Laser Diode Current/TEC Controller ±500 mA / ±1.5 A
- ITC5102: Laser Diode Current/TEC Controller ±1 A / ±1.5 A

#### ITC5000 Features

- · Laser Diode Current and Temperature Control
- · Very Low Noise and Drift
- Excellent Temperature Stability
- · Supports All Laser Diode and Monitor Diode Polarities
- Constant Current (CC) and Constant Power (CP) Modes
- · Superior Laser Diode Protection
- Internal & External Modulation
- Safe & Ultra-Stable Laser Diode Operation

#### ntroduction

The ITC5000 Series Modules are combination laser diode and TEC controllers for the TXP platform. They allow space-saving simultaneous current and temperature control of a laser diode with a single module. The ITC5000 Series offers three laser diode current ranges, ±200 mA, ±500 mA and ±1 A, that support all laser diode and monitor diode polarities. These modules can also be modulated, externally or internally. All three models incorporate a TEC controller that provides up to ±1.5 A / 5.25 W.

#### Features

Besides common protection functions such as interlock and softstart, an advanced circuit design ensures that transient spikes cannot affect the laser current. The temperature controller, which is identical for all modules, is designed to keep the laser temperature constant for highly stable power and wavelength operation. Separate adjustment of the P, I and D shares of the temperature servo loop allow optimizing temperature settling times. An additional temperature

window protection circuit switches the laser current off if the laser temperature leaves a preset temperature window.

The ITC5000 models offer exceptional noise and stability performance. All laser diode and photodiode pin configurations are supported.

#### Operation

For the operation of the **ITC5000** modules a TXP chassis is required. The modules are hot-pluggable, i.e. you can insert or remove them during operation of other modules. An intuitive graphical user interface (GUI) for the **ITC5000** is delivered with the TXP chassis, as well as drivers for LabVIEW™, LabWindows/CVI™, MSVC and Borland C.

#### **Connection Cables**

A CAB530 cable is required to connect the ITC5000 modules to a Thorlabs' Laser Diode Mount. The cable has to be ordered separately.

For further information, please contact our Tech Support Team.

Laser Diode Accessory Selection Guide						
Temperature Controlled Mounts	Passive Mounts	Passive Mounts with Collimation Package Strain Relief Cables Diode Sockets Other Controllers				
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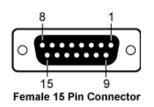
### Hide Specs

PECS				
Item #	ITC5022	ITC5052	ITC5102	
Laser Controller: Current Control				
Control Range (continuous)	0 to ±200 mA	0 to ±500 mA	0 to ±1 A	
Compliance Voltage		>2.5 V (typ. >3 V)		
Resolution	4 μΑ	10 μA	20 μΑ	
Accuracy (typ., f.s.)	±100 μA	±250 μA	±1 mA	
Noise without Ripple (10Hz to 10MHz, RMS, typ.)	<2 μA	<7 μΑ	<20 μA	
Ripple (50Hz / 60Hz, RMS, typ.)		<0.5 μΑ		
Transients (Processor, typ.)	<15 μΑ	<30 μΑ	<50 μΑ	
Transients (other, typ.)	200 μΑ	500 μA	1 mA	
Drift (24hrs, at constant ambient temperature, typ.)	<2 μA	<5 μA	<20 μA	
Temperature Coefficient		<50 ppm/°C		
Laser Controller: Power Control				
Control Range of Photo Current		10 μA to 5 mA		
Resolution		0.1 μΑ		
Accuracy (typ., f.s.)		±5 μA		
Reverse Bias Voltage		0 to 4 V (adjustable)		
Laser Controller: Current Limit				
Setting Range	0 to >200 mA	0 to >500 mA	0 to >1 A	
Resolution	50 μA	125 µA	250 μΑ	
Accuracy (typ., f.s.)	±200 μA	±500 μA	±2 mA	
Laser Voltage Measurement				
Measurement Principle	4-Wire (improve	4-Wire (improves accuracy by compensating for cable resistance)		
Measurement Range		0 to 4 V		
Resolution		0.15 mV		
Accuracy		±5 mV		
External Laser Modulation				
Input Resistance		10 kΩ		

Modulation Coefficient (Constant Current Mode)	20 mA/V ± 10% 50 mA/V ± 10%	100 mA/V ± 10%			
3 dB Modulation Bandwidth (Constant Current Mode)	200 kHz	200 kHz			
Modulation Coefficient (Constant Power Mode)	0.5 mA/V ± 10%				
Internal Laser Modulation					
Format	Sinusoidal, Triangular,	Square			
Frequency Range	0.02 to 20 kHz	!			
Rise-/Fall Time>	4 µs				
Temperature Controller: Output					
Control Range of TEC Current	-1.5 A to +1.5 A	4			
Compliance Voltage	>3.5 V				
Maximum Output Power	5.25 W				
Measurement Resolution TEC Current	60 μΑ				
Measurement Range TEC Voltage	-4 V to +4 V				
Measurement Resolution TEC Voltage	0.2 mV				
Noise and Ripple (typ.)>	<1 mA				
Temperature Controller: Measurement Sensor					
Sensor Type	Thermistor				
Operating Range	0.2 to 40 kΩ				
Resolution	0.8 Ω				
Accuracy	±10 Ω				
Stability (24hrs)	1 Ω				
Temperature Control Loop	'				
Туре	PID, analog				
Resolution P/I/D-Share Setting	12 Bit each				
TEC Current Limit					
Adjustment Range	0 to >1.5 A				
Resolution via D/A Converter	0.5 mA				
Accuracy	±20 mA				
General Data					
Protection Features	Global and Local Into Output Short Circuit when Laser Softstart, Laser Tempe Laser and TEC Current Limits, Ope No Sensor Detection, Over Temp	n Laser off, rature Window, en Output Detection,			
Connector Laser / TEC	15-pin D-Sub				
Connector Modulation Input	SMA				
Card Width	1 TXP Slot				
Dimensions (W x G x D)	25 mm x 130 mm x 2	70mm³			
Weight	675 g				
Operating Temperature	0 to 40 °C				
Storage Temperature	-40 to 70 °C				
Warm-up Time	<10 min				
All technical data are y	alid at 23 ± 5 °C and 45 ± 15% relative humidity				

All technical data are valid at 23  $\pm$  5  $^{\circ}\text{C}$  and 45  $\pm$  15% relative humidity.

### Hide Pin Diagrams



Pin	Connection	Pin	Connection
1	Interlock/Status LED (LED_ILK)	9	Laser Diode Voltage Measurement (ULD-)
2	Monitor Diode Ground/Bias Ground (PD_GND)	10	Laser Diode Cathode (LDK)
3	Laser Diode Ground (LGND)	11	Laser Diode Anode (LDA)
4	Monitor Diode Anode or Cathode, Bias Out (PD_BIAS)		Laser Diode Voltage Measurement (ULD+)
5	Interlock Ground (DGND)	13	TEC Voltage Measurement (-) UTEC-
6	6 TEC Voltage Measurement (+) UTEC+		Thermistor Ground (TH-)
7	TEC Plus (TEC +)	15	Thermieter (TU+)
8	TEC Minus (Ground) (TEC -)	15	Thermistor (TH+)

### **External Modulation via SMA**

### SMA Female



Voltage Range 0 - 10 V

### Hide Software

### SOFTWARE

The Software Package for the TXP5000 Platform contains the Software Modules for the ITC5000 Series

### **TXP Software**

Version 3.1.5

Standard full TXP software packages for the ITC5000 Series: Applications, Drivers, and Firmware.



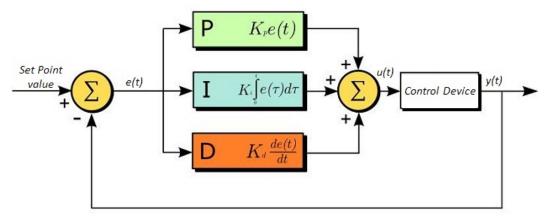
### Hide Shipping List

### SHIPPING LIST

ITC5022	ITC5052	ITC5102	Part
х			Laser Diode Current/TEC Controller ±200 mA / ±1.5 A (ITC5022)
	х		Laser Diode Current/TEC Controller ±500 mA / ±1.5 A (ITC5052)
		х	Laser Diode Current/TEC Controller ±1 A / ±1.5 A (ITC5102)
х	х	х	Operating Manual

#### **PID Basics**

The PID circuit is often utilized as a control loop feedback controller and is very commonly used for many forms of servo circuits. The letters making up the acronym PID correspond to Proportional (P), Integral (I), and Derivative (D), which represents the three control settings of a PID circuit. The purpose of any servo circuit is to hold the system at a predetermined value (set point) for long periods of time. The PID circuit actively controls the system so as to hold it at the set point by generating an error signal that is essentially the difference between the set point and the current value. The three controls relate to the time-dependent error signal; at its simplest, this can be thought of as follows: Proportional is dependent upon the present error, Integral is dependent upon the accumulation of past error, and Derivative is the prediction of future error. The results of each of the controls are then fed into a weighted sum, which then adjusts the output of the circuit, u(t). This output is fed into a control device, its value is fed back into the circuit, and the process is allowed to actively stabilize the circuit's output to reach and hold at the set point value. The block diagram below illustrates very simply the action of a PID circuit. One or more of the controls can be utilized in any servo circuit depending on system demand and requirement (i.e., P, I, PI, PD, or PID).



Through proper setting of the controls in a PID circuit, relatively quick response with minimal overshoot (passing the set point value) and ringing (oscillation about the set point value) can be achieved. Let's take as an example a temperature servo, such as that for temperature stabilization of a laser diode. The PID circuit will ultimately servo the current to a Thermo Electric Cooler (TEC) (often times through control of the gate voltage on an FET). Under this example, the current is referred to as the Manipulated Variable (MV). A thermistor is used to monitor the temperature of the laser diode, and the voltage over the thermistor is used as the Process Variable (PV). The Set Point (SP) voltage is set to correspond to the desired temperature. The error signal, e(t), is then just the difference between the SP and PV. A PID controller will generate the error signal and then change the MV to reach the desired result. If, for instance, e(t) states that the laser diode is too hot, the circuit will allow more current to flow through the TEC (proportional control). Since proportional control is proportional to e(t), it may not cool the laser diode quickly enough. In that event, the circuit will further increase the amount of current through the TEC (integral control) by looking at the previous errors and adjusting the output in order to reach the desired value. As the SP is reached [e(t) approaches zero], the circuit will decrease the current through the TEC in anticipation of reaching the SP (derivative control).

Please note that a PID circuit will not guarantee optimal control. Improper setting of the PID controls can cause the circuit to oscillate significantly and lead to instability in control. It is up to the user to properly adjust the PID gains to ensure proper performance.

#### **PID Theory**

The output of the PID control circuit, u(t), is given as

$$u(t) = MV(t) = K_p e(t) + K_i \int_0^t e(\tau) d\tau + K_d \frac{d}{dt} e(t)$$

where

K<sub>p</sub>= Proportional Gain

K<sub>i</sub> = Integral Gain

K<sub>d</sub> = Derivative Gain

e(t) = SP - PV(t)

From here we can define the control units through their mathematical definition and discuss each in a little more detail. Proportional control is proportional to the error signal; as such, it is a direct response to the error signal generated by the circuit:

$$P = K_p e(t)$$

Larger proportional gain results is larger changes in response to the error, and thus affects the speed at which the controller can respond to changes in the

system. While a high proportional gain can cause a circuit to respond swiftly, too high a value can cause oscillations about the SP value. Too low a value and the circuit cannot efficiently respond to changes in the system.

Integral control goes a step further than proportional gain, as it is proportional to not just the magnitude of the error signal but also the duration of the error.

$$I = K_i \int_0^t e(\tau) d\tau$$

Integral control is highly effective at increasing the response time of a circuit along with eliminating the steady-state error associated with purely proportional control. In essence integral control sums over the previous error, which was not corrected, and then multiplies that error by  $K_i$  to produce the integral

response. Thus, for even small sustained error, a large aggregated integral response can be realized. However, due to the fast response of integral control, high gain values can cause significant overshoot of the SP value and lead to oscillation and instability. Too low and the circuit will be significantly slower in responding to changes in the system.

Derivative control attempts to reduce the overshoot and ringing potential from proportional and integral control. It determines how quickly the circuit is changing over time (by looking at the derivative of the error signal) and multiplies it by  $K_d$  to produce the derivative response.

$$D = K_d \frac{d}{dt} e(t)$$

Unlike proportional and integral control, derivative control will slow the response of the circuit. In doing so, it is able to partially compensate for the overshoot as well as damp out any oscillations caused by integral and proportional control. High gain values cause the circuit to respond very slowly and can leave one susceptible to noise and high frequency oscillation (as the circuit becomes too slow to respond quickly). Too low and the circuit is prone to overshooting the SP value. However, in some cases overshooting the SP value by any significant amount must be avoided and thus a higher derivative gain (along with lower proportional gain) can be used. The chart below explains the effects of increasing the gain of any one of the parameters independently.

Parameter Increased	Rise Time	Overshoot	Settling Time	Steady-State Error	Stability
K <sub>p</sub>	Decrease	Increase	Small Change	Decrease	Degrade
K <sub>i</sub>	Decrease	Increase	Increase	Decrease Significantly	Degrade
K <sub>d</sub>	Minor Decrease	Minor Decrease	Minor Decrease	No Effect	Improve (for small K <sub>d</sub> )

#### **Tuning**

In general the gains of P, I, and D will need to be adjusted by the user in order to best servo the system. While there is not a static set of rules for what the values should be for any specific system, following the general procedures should help in tuning a circuit to match one's system and environment. In general a PID circuit will typically overshoot the SP value slightly and then quickly damp out to reach the SP value.

Manual tuning of the gain settings is the simplest method for setting the PID controls. However, this procedure is done actively (the PID controller turned on and properly attached to the system) and requires some amount of experience to fully integrate. To tune your PID controller manually, first the integral and derivative gains are set to zero. Increase the proportional gain until you observe oscillation in the output. Your proportional gain should then be set to roughly half this value. After the proportional gain is set, increase the integral gain until any offset is corrected for on a time scale appropriate for your system. If you increase this gain too much, you will observe significant overshoot of the SP value and instability in the circuit. Once the integral gain is set, the derivative gain can then be increased. Derivative gain will reduce overshoot and damp the system quickly to the SP value. If you increase the derivative gain too much, you will see large overshoot (due to the circuit being too slow to respond). By playing with the gain settings, you can maximize the performance of your PID circuit, resulting in a circuit that quickly responds to changes in the system and effectively damps out oscillation about the SP value.

While manual tuning can be very effective at setting a PID circuit for your specific system, it does require some amount of experience and understanding of PID circuits and response. The Ziegler-Nichols method for PID tuning offers a bit more structured guide to setting PID values. Again, you'll want to set the integral and derivative gain to zero. Increase the proportional gain until the circuit starts to oscillate. We will call this gain level  $K_u$ . The oscillation will have a period of  $P_u$ . Gains are for various control circuits are then given below in the chart.

Control Type	К <sub>р</sub>	K <sub>i</sub>	K <sub>d</sub>
Р	0.50 K <sub>u</sub>	-	-
PI	0.45 K <sub>u</sub>	1.2 K <sub>p</sub> /P <sub>u</sub>	-
PID	0.60 K <sub>u</sub>	2 K <sub>p</sub> /P <sub>u</sub>	K <sub>p</sub> P <sub>u</sub> /8

Description	Price	Availability
Laser Diode Current/TEC Controller ±200mA / 1.5A	\$2,257.74	Lead Time
Laser Diode Current/TEC Controller ±500mA / 1.5A	\$2,257.74	Lead Time
Laser Diode Current/TEC Controller ±1A / 1.5A	\$2,257.74	Lead Time
	Laser Diode Current/TEC Controller ±200mA / 1.5A  Laser Diode Current/TEC Controller ±500mA / 1.5A	Laser Diode Current/TEC Controller ±200mA / 1.5A \$2,257.74  Laser Diode Current/TEC Controller ±500mA / 1.5A \$2,257.74

### Hide Connection Cable for the ITC5000 Series

## Connection Cable for the ITC5000 Series



Pin #	CAB530 (15 Pin)	CAB530 (9 Pin)	CAB530 (9 Pin)
	9 15 Male 15 Pin Connector	Male 9 Pin Connector	5 1 0 9 6 Female 9 Pin Connector
1	Interlock and Status LASER ON/OFF	Interlock and Status LASER ON/OFF	N.C.
2	Photodiode Ground, Cathode or Anode (configurable)	Photodiode Ground, Cathode or Anode (configurable)	Thermistor (+)
3	Laser Diode Ground	Laser Diode Ground	Thermistor (-), Ground
4	Photodiode Input, Anode or Cathode (configurable)	Photodiode Input, Anode or Cathode (configurable)	TEC (+)
5	Ground for Pin 1	Ground for Pin 1	TEC (-), Status LED (-)
6	Voltage Measurement TEC (+)	Voltage Measurement Laser Diode Cathode	N.C.
7	TEC (+)	Laser Diode Cathode (with Polarity Anode Grounded - AG)	N.C.
8	TEC (-)	Laser Diode Anode (with Polarity Cathode Grounded - CG)	N.C.
9	Voltage Measurement Laser Diode Cathode	Voltage Measurement Laser Diode Anode	N.C.
10	Laser Diode Cathode (with Polarity Anode Grounded - AG)		
11	Laser Diode Anode (with Polarity Cathode Grounded - CG)		
12	Voltage Measurement Laser Diode Anode		
13	Voltage Measurement TEC (-)		
14	Thermistor (-), Ground		
15	Thermistor (+)		

Part Number	Description	Price	Availability
CAB530	Cable for a ITC5000 series card to Thorlabs TEC Laser Diode Mounts	\$102.96	Today